

TRACE ANALYSIS AND ULTRAPURIFICATION OF MATERIALS FOR OPTICAL WAVEGUIDE TECHNOLOGY

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Abstract - In the telecommunications industry techniques for purifying and characterizing materials, and analytical methods for solving chemical problems have been vitally important for technological progress. The application of reliable analytical methods to determine optimum conditions for preparing materials in controlled states of purity continues to be essential. In fact, the production of materials with unique properties, determined by doping precisely with impurities on the one hand or by insuring the absence of other detrimental ones, continues to be a key to technological advancement.

The most recent critical need in the industry for pure materials and ultratrace analysis resulted from the initiation of applied research and development of optical waveguide systems, where tolerance limits for waveguide materials were projected to be in the 2 to 100 ng/g range for commonly found transition metal impurities Fe, Co, Cr, Cu, Mn, Ni, and V. Applications of neutron activation, X-ray fluorescence, atomic absorption, and laser intracavity absorption spectroscopy in support of optical waveguide programs will be discussed. Examples will be provided to demonstrate the use of these techniques for screening commercially available glass-making raw materials and chemical vapor deposition reagents, for unequivocally identifying impurities in glasses and fibers, and for detecting sources of contamination during glass-making and fiberdrawing.

In the absence of materials of sufficient purity from available commercial sources, specialized preparations have been performed under controlled executions of solvent extraction, ion exchange, mercury cathode electrolysis, and low temperature sublimation. The advantages and pitfalls of these methods will be compared. It will be demonstrated that radioisotope techniques and activation analysis are the most powerful and reliable tools for establishing optimum conditions for executing these procedures and for pinpointing specific deficiencies of each purification process. Factors limiting the ultimate state of purity achievable for analytical reagents for trace analysis will be discussed.

INTRODUCTION

Many industries in the United States are quite dependent upon analytical chemistry for their growth and ultimate success. The communication industry provides a particular example where techniques for purifying and characterizing materials, and methods for solving chemical problems have been vitally important for technological advancements. As is now well recognized the first real revolution in communication technology followed the development of zone refining techniques at Bell Laboratories. This process made it possible to prepare extremely pure silicon, germanium, and other materials from which semiconductor devices could be processed. Soon after this discovery materials were fabricated with such high degrees of purity that trace elements could not be easily detected by existing analytical methods. Thus electrical tests, such as resistivity and others were used. Although these electrical methods were very useful, they were nonspecific; and it was not

possible to identify the impurities present. As a result, analytical research to develop extremely sensitive, specific methods was stimulated and has continued to be a primary factor essential in technological research and development.

As is already evident instrumental and chemical methods for trace analysis have been developed and applied to a wide variety of materials characterization problems. Many materials in controlled states of purity are required for fabricating various components of telecommunications systems. In fact the production of materials with important properties has been one of the keys to technological advancement in the communications industry. A few examples of materials and important properties are listed in Table 1.

TABLE 1. Materials required in controlled states of purity

<u>Material</u>	<u>Application</u>	<u>Controlled Impurities</u>
{ Silicon	{ Device production	Defects, Na, B, P, Cl, As, O, Al
{ Germanium	{ Radiation detectors	
Fused silica	Containers, fiber optic cladding	Transition elements (Tr,M's)
MCVD preforms	Optical fibers	Fe, Cu, Ni, Cr, Mn, Co, -OH
GaP, GaAs	LED's , Lasers	O, C, N, Cl, P, other Tr.M's
Quartz	Piezoelectric resonators	Fe, Al, -OH
Platinum	Containers	Fe, Ir
Gold	Plating	Fe, Sn, Pb, C
Cu-Ni-Sn	Spring alloys	P, Pb, Ti, Si, Y
{ Graphite	{ Varister manufacture	Al, Fe
{ Silicon carbide		

The properties of some materials change dramatically with impurity content and with variation in composition. Low ppb levels of certain impurities in semiconductors and glass will render the material completely useless for the intended application while certain properties are only obtained by precisely doping materials with known amounts of important trace elements.

The most recent critical need in the telecommunications industry for pure materials and trace element analyses occurred with the initiation of research to develop optical waveguide systems. Although today's telephone systems depend largely on transmission of electrical signals via copper conductor cables, systems of the future will be based on combinations of electrical and optical transmission components. A schematic diagram of a representative optical waveguide cable is shown in Fig. 1.

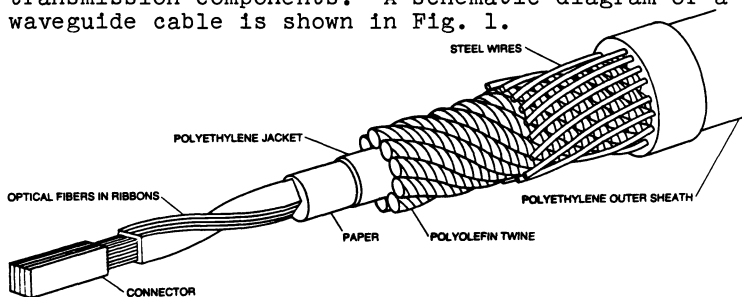


Fig. 1. Optical waveguide cable system

An optical waveguide is essentially a light pipe into which light of appropriate characteristics is launched from a suitable LED or laser source and then is propagated through the fiber via total internal reflection from the core-cladding interface. Because the transmission bandwidth capacity of the fiber is extremely large and its physical dimensions exceedingly small in comparison to other systems in use today, the worldwide telecommunications industry is very active in applied research, development and deployment of optical waveguide systems.

Glass has emerged as the most suitable material for fabricating optical waveguides. To be useful for this purpose the material must be devoid of impurities that would attenuate the propagating light via absorption losses. Projected tolerance limits for certain transition elements in glasses of various composition are given in Table 2.

TABLE 2. Impurity levels (PPB) introducing 1 dB/Km absorption losses at 800 nm in various glasses

<u>Impurity</u>	<u>Na-Ca-Si</u>	<u>SiO₂</u>	<u>Na-B-Si</u>
Co	0.2	40	100
Cr	2.1	2	20
Cu	5.1	100	1(II)*, 10(I)*
Fe	2.1	20	1(II)*, 1000(III)*
Mn	10.1	50	100
Ni	2.1	40	10
V	10.1	1	25

* (I), (II), (III) are oxidation states of impurities

SCOPE AND OBJECTIVES OF ANALYTICAL PROGRAM

The analytical information required for supporting the waveguide research program included, rapid screening of available glasses and glassmaking raw materials to determine their suitability for waveguide production, identifying impurities present in these materials, detecting sources of contamination during glassmaking and fiber drawing, and developing procedures for preparing materials of sufficient purity in the event commercially available products were too impure. To obtain this information extremely sensitive and reliable quantitative methods were required since small changes in the levels of various traces would need to be distinguished. The appropriate support method could be chosen from the listing of analytical techniques in Table 3. Neutron activation analysis (NAA) was selected as the primary support method because of its characteristic features of [1] sufficient sensitivity for direct sub-ppm and sub-ppb detection of a large number of trace elements, [2] application for rapid, semi-quantitative survey determinations of a large number of elements or highly accurate, selective, single element determinations using chemical separations, and [3] freedom from blank problems that could occur during post-irradiation chemical processing of the sample. X-ray fluorescence (XRF), atomic absorption spectroscopy (AAS), and laser intracavity absorption spectrophotometry have also been applied.

TABLE 3. Techniques for trace and ultratrace analysis

Atomic absorption spectroscopy (AAS)
 Atomic fluorescence spectroscopy (AFS)
 Coulometric titration
 Electron-capture gas-liquid chromatography
 Electronprobe microanalysis
 Emission spectroscopy (ES)

Fluorimetry
 Ion-specific electrodes
 Kinetic measurements
 Mass spectroscopy (MS)
 Neutron activation (NAA)
 Nuclear track counting
 Polarography
 Radioisotope dilution (RID)
 RF induction coupled atomic emission
 Stable isotope dilution (SID)
 Spectrophotometry
 Titrimetric methods
 X-ray fluorescence (XRF)

SURVEYS OF THE PURITY OF COMMERCIALY AVAILABLE MATERIALS

Neutron activation with gamma-ray spectroscopy was used to screen commercial samples of sodium and calcium carbonate to detect Fe, Cr, and Co impurities. Inspection of gamma-ray spectra is used to select the most pure compound in a series of samples irradiated simultaneously. Sample A in Fig. 2 is clearly the most pure product with respect to impurities of interest.

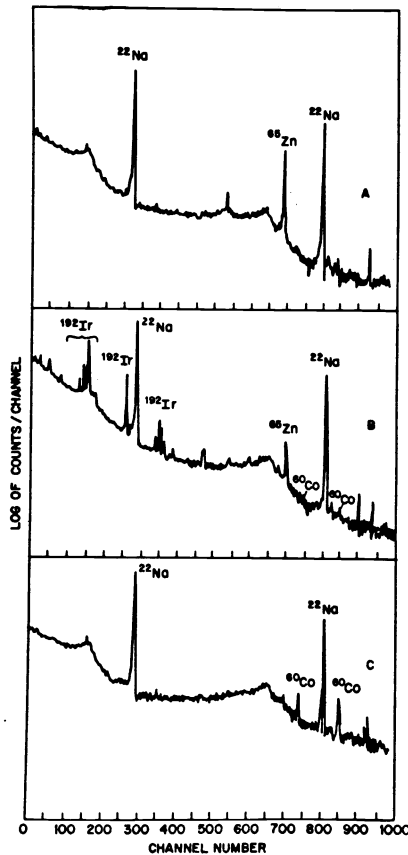


Fig. 2. Gamma-ray spectra of sodium carbonates.

Spectra of CaCO_3 samples distributed by suppliers of lightguide materials are shown in Fig. 3. Characteristic photopeaks, for ^{60}Co , ^{51}Cr , and ^{46}Sc are present in Sample B.

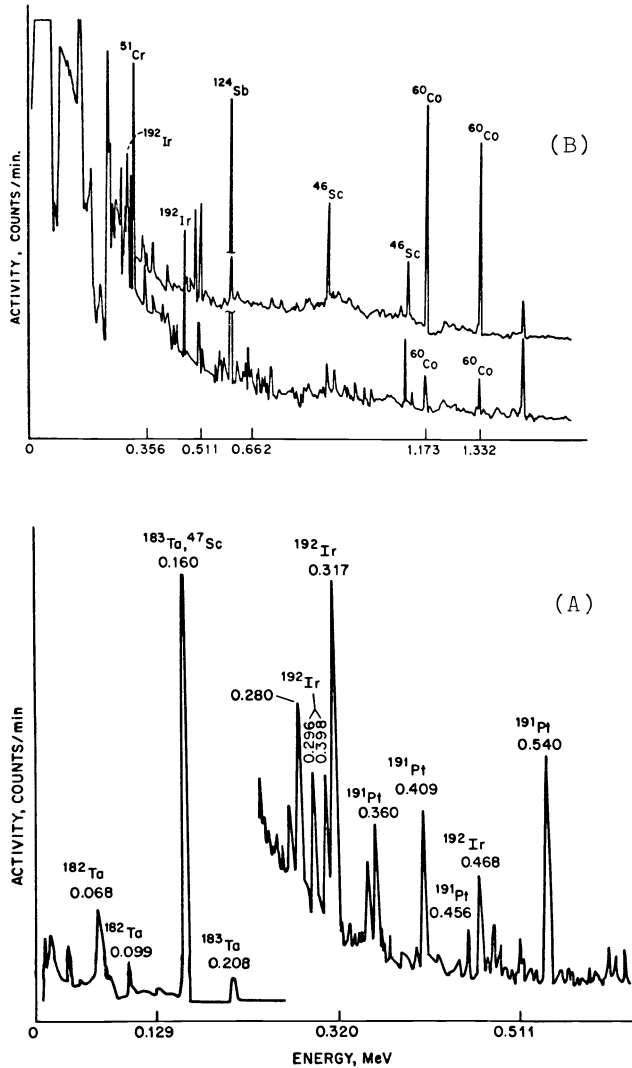


Fig. 3. Gamma-ray spectra of calcium carbonate.

Additional impurities in Sample A include full energy peaks for ^{182}Ta , ^{183}Ta , ^{192}Ir , ^{191}Pt , and $^{195\text{m}}\text{Pt}$. The detection of ^{191}Pt ($T_{1/2} = 3.00\text{d}$) after a 13d decay period showed considerable contamination by this rare trace element. This was subsequently related to the use of platinum containers for thermal decomposition of a high-purity precursor compound to obtain calcium carbonate. Iridium, an additive of platinum to increase hardness, is detected with very high sensitivity. Because of its large cross section and long half-life, detection of this isotope serves as a sensitive probe to determine contamination from platinum containers.

Similar instrumental analyses by γ -ray spectroscopy to perform semiquantitative analyses of available silica showed degrees of purity represented by the data in Table 4. These initial surveys of readily available glass-making raw materials showed them to be insufficiently pure for optical waveguide use. In the case of silica, the semiquantitative survey reported in Table 4 indicated that Fe contamination in all of the commercially available powdered silica exceed tolerance limits. Although synthetic fused silica rods (Suprasil) were the purest form of silica available commercially and appeared to meet specifications for most elements, powdered starting materials were required for the production of bulk glass by melting techniques.

TABLE 4. Detection of trace elements in silica^a

<u>Supplier</u>	<u>Concentration $\mu\text{g/g}$</u>		
	<u>Fe</u>	<u>Co</u>	<u>Cr</u>
(1)	1.24	0.030	1.90
(2)	0.82	0.005	2.16
(3)	1.60	0.041	0.17
(4)	1.00	0.008	0.19
(5)	0.68	0.009	0.009
Suprasil	ND	ND	ND
	<0.1	<0.003	<0.005

^aSemiquantitative γ -ray spectrometric surveys using synthetic comparison standards

PURIFICATION METHODS

When readily available commercial raw materials are not sufficiently pure to meet waveguide tolerance limits for trace impurities, materials of sufficient purity must be prepared specifically. This project was attacked by a special task force consisting of purification specialists and analytical chemists with expertise in quantitative, ultratrace, inorganic analyses. Appropriate purification schemes had to be devised and evaluated for producing the desired reagent. Radioisotope techniques and activation analyses were powerful tools for establishing optimum conditions for executing the procedure and for pinpointing specific deficiencies of each step of the purification process.

Solvent extraction

Solvent extraction is an excellent method for preliminary purification of reagent grade solutions of sodium or calcium. The efficiency of step A (Fig. 4) was evaluated by measuring distribution ratios for Cu, Fe, Cr, Mn, Co, and V using appropriate radioisotopes. The measured distribution ratios and the corresponding data showing percentage extraction results indicated excellent removal of trace quantities of Mn, Co, Fe, and Cu from sodium feed solutions. but the distribution ratios for Cr^{3+} and VO_2^+ were low. Cr^{3+} could not be 100% extracted with a 0.2% solution of pyrrolidinedithiocarbamic acid (HPDC) in CHCl_3 (6N HCl to pH 3.04), with dithizone, or with 0.01-0.1 M 8-hydroxyquinoline in CHCl_3 at any pH.

Other investigations with radiotracers aided in evaluating solvent extraction methods for preparing ultrapure calcium carbonate. Multiple extraction of 5.0 M calcium nitrate solutions with CHCl_3 containing 1% dithiocarbamate showed effective removal of ng/ml amounts of Fe^{3+} and Mn^{2+} . Distribution ratios at pH 7.4 were ~ 14 and 900 respectively. This extraction system was used effectively to decontaminate calcium solution containing Mn impurities. Samples of an original and extracted calcium solution were irradiated. ^{56}Mn and ^{64}Cu were separated simultaneously by extraction into CHCl_3 solutions of 8% HPDC-0.12% dithizone. Results by activation analysis showed 109 ± 10 ng and <0.1 ng of Mn in the original and purified solutions. Copper was below detection limits in both samples.

Ion exchange

Ion exchange procedures are very effective for removal of ultratrace impurities. A flow diagram of a procedure for preparing sodium carbonate is shown in Fig. 4. Procedures of this kind require many handling steps and chemical manipulations. Therefore, extreme care is necessary to minimize contamination from containers and to ensure that the most pure chemical reagents are used. Other major sources of impurities, for example, the reagent grade NaNO_3 feed solution and exchangeable cationic impurities on the Amberlite IR 120 resin, must be recognized and minimized. Steps A and C were designed to purify the feed solution and to remove impurities from the loaded ion exchange resin. Ion exchange resins were also purified by elution with

EDTA prior to loading with feed solutions.

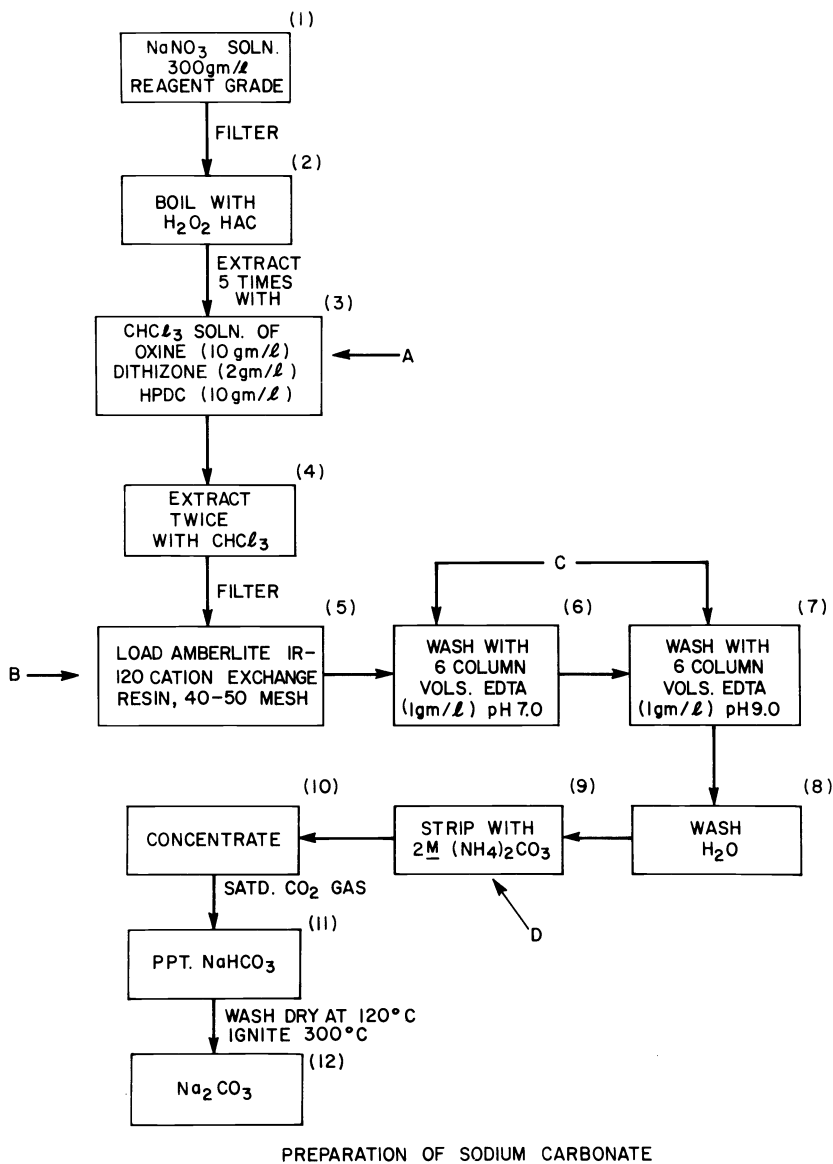


Fig. 4. Solvent extraction and ion exchange scheme for purifying sodium solutions

The effectiveness of the entire procedure for removing submicrogram/ml amounts of Fe, Mn, Cu, Cr, Co, and V was determined by radioisotope techniques. One portion of a prepurified sodium nitrate feed solution was doped with carrier-free or high-specific activity ^{59}Fe , ^{54}Mn , ^{51}Cr , and ^{60}Co and the second aliquot with ^{64}Cu and $^{48}\text{VO}_2^+$. The effectiveness of each step of the procedure from the purification of the feed solution by solvent extraction (A) to stripping of the loaded sodium resin with 2M ammonium carbonate (D) have been examined and detailed experimental procedures and important results of this investigation are reported elsewhere (Ref. 1).

Mercury cathode electrolysis

Methods based on mercury cathode electrolysis have been perfected as final processes for decontaminating sodium and calcium solutions (Ref. 2). The development of the successful procedure for preparing large quantities of the material depended ultimately on effective analytical support. Small 100g test samples of CaCO_3 (1 and 2 Table 5) were obtained for evaluation of purity prior to the beginning of large scale preparations. Neutron activation results for Mn and Cu showed test samples to pass specifications for

these traces.

TABLE 5. NAA determination of Mn and Cu in CaCO_3

Sample	Conc. found, ng/g	
	Cu	Mn
1 ^a	N.D. ^b	43.8 ± 7.8
2	26 ± 6	29.8 ± 1.0
3	N.D.	340 ± 9.0
4	38 ± 5	523 ± 12
5	N.D.	658 ± 13

^a 4 detn., ^b not detected.

When kilogram quantities of the reagent were supplied (samples 3, 4 and 5) the level of contamination by manganese made the material unsuitable. Optimization of the conditions for purification of solutions by mercury cathode electrolysis has been accomplished by applications of radioisotope techniques (Ref. 3). The simultaneous γ -ray spectrometric monitoring of the removal of impurities from sodium carbonate solutions is shown in Fig. 5.

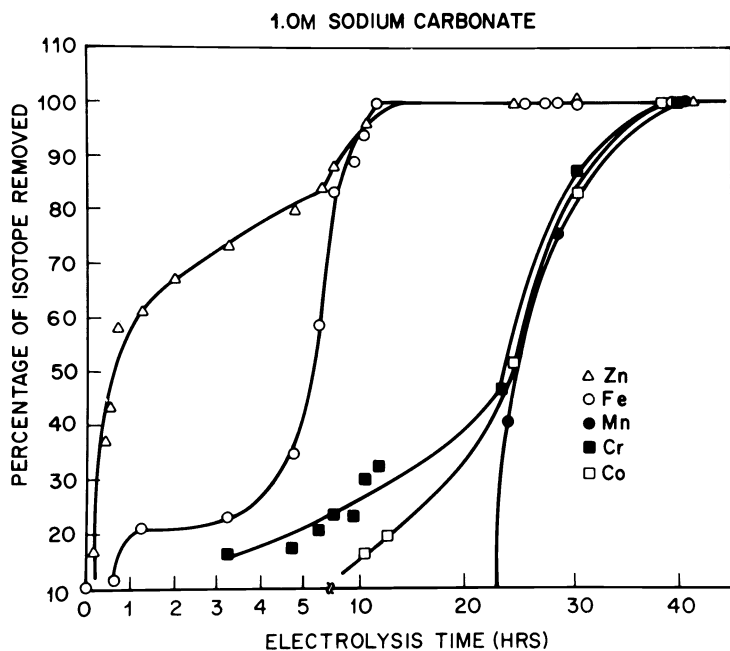


Fig. 5. Gamma-ray spectrometric monitoring of the mercury cathode electrolysis purification of sodium carbonate solutions

Data from these types of studies and that obtained via direct monitoring of the Mn levels in samples periodically removed during the electrolysis of non-isotope doped solutions pinpointed the pH and electrolysis time periods

required for efficient removal of ultralow levels of manganese. Accurate control of the pH and time of electrolysis resulted in large scale preparation of calcium carbonate which passed the specification for manganese. An additional essential factor in ultrapurification was adequate control of particulate contamination. XRF and AAS techniques disclosed the significant contribution of particulate contamination to the total transition element content of the final product (Ref. 4).

Low temperature sublimation

New technology for optical waveguide production has exploited the vapor phase oxidation of gaseous molecules, for example SiCl_4 , GeCl_4 , POCl_3 and BCl_3 , inside fused silica tubes as a process for producing glass (Ref. 5). This modified chemical vapor deposition (MCVD) process (Ref. 6) thus stimulated the development of additional methods for the purification and analysis of CVD reagents. An extremely effective low temperature sublimation technique was developed for the ultrapurification of a number of important liquids used as either analytical or MCVD reagents (Table 6).

TABLE 6. Desirable ultrapure reagents

For analytical chemistry

Hydrogen peroxide	H_2O_2
Hydrazine	NH_2NH_2

For chemical vapor deposition

Phosphorus oxychloride	POCl_3
Antimony pentachloride	SbCl_5
Phosphorus tribromide	PBr_3
Arsenic trichloride	AsCl_3
Tungsten hexafluoride	WF_6
Silicon tetrachloride	SiCl_4
Germanium tetrachloride	GeCl_4
Boron trichloride	BCl_3

Experimental verification of the extremely high efficiency of the method for the purification of hydrogen peroxide was reported previously (Ref. 7). Analytical results for the purification of a number of important chemical reagents is given in Table 7. The low temperature sublimation technique is now applied for the batch-scale production of kilogram quantities of MCVD reagents

QUANTITATIVE ANALYSIS OF HIGH PURITY MATERIALS

The production of ultrapure reagents depended critically on high sensitivity and very reliable quantitative analyses. To obtain the required information chemical separations and procedures for post irradiation processing of raw materials were devised. The radionuclidic interference from ^{24}Na during the determination of Cu and Mn in sodium carbonate was eliminated by passing carrier-doped solution through hydrated antimony pentoxide (HAP) columns to remove ^{24}Na . Interferences from other matrix isotopes are eliminated by simultaneously extracting ^{64}Cu and ^{55}Mn at pH 6 to 8 into CHCl_3 containing 1% pyrrolidine dithiocarbamic acid and 0.01% dithizone (Ref. 8). Cu and Mn in samples of calcium carbonate have been determined in a similar manner. It was not necessary to remove high levels of ^{24}Na with the HAP column since the organic extracts of dissolved calcium carbonates contained only low background activity from this matrix isotope.

The reliability of procedures has been assessed by performing replicate analyses (6 determinations) of synthetic standard solutions prepared by

dissolving extremely pure sodium carbonate ($[Cu] = 18.9 \pm 7 \text{ ng/g}$, $[Mn] = 3.3 \pm 0.7 \text{ ng/g}$) and doping with with $1.00 \text{ } \mu\text{g/ml}$ of Cu and $0.1107 \text{ } \mu\text{g/ml}$ of Mn. The results, 0.992 ± 0.055 , and $0.1050 \pm 0.035 \text{ } \mu\text{g/ml}$ for Cu and Mn respectively indicate errors of 0.8 and 5.3%. Measurable detection limits of 0.3 and 0.03 ng were obtained for Cu and Mn respectively under conditions of 15 min. counting intervals on a 9% efficient sodium iodide well-type detector.

TABLE 7. Results of single sublimations (concn ng/ml)

Impurity	Hydrogen ^A Peroxide		Phosphorus ^B Oxychloride		Hydrazine ^B	
	Before	After	Before	After	Before	After
Co	1000	0.4	< 0.4	N.D. ^C	40	N.D.
Cr	1000	< 2	28	N.D.	127	N.D.
Cu	1000	< 2	N.D.	-	3.0	0.3
Fe	1000	< 2	433 ± 6	23 ± 8	41	2.0
Mn	1000	0.9	14	N.D.	2.0	N.D.
Ni	1000	-	1245 ± 70	N.D.(<1)	13	N.D.

^AAnalyzed by radiosotope method, ^BAnalyzed by atomic absorption.

^CN.D. = below detection limits.

For determinations of manganese in calcium carbonates a new substoichiometric method was developed (Ref. 9). With this method highly sensitive, precise analyses with good accuracy were obtained as indicated by the mean of five determinations, $0.151 \pm 0.009 \text{ } \mu\text{g}$. Comparison of the determined value with that calculated from the recommended SRM value, $0.17 \pm 0.013 \text{ } \mu\text{g}$, indicated an absolute error of 5.9 to 11.7% for the determination of Mn at the 0.2 μg level.

Additional data on calcium carbonate purity with respect to Cu and Mn are given in Table 5. Other trace elements in sodium carbonate with long lived isotopes, ^{60}Co , ^{51}Cr , and ^{59}Fe , for example, can be measured instrumentally following 100 hr. irradiations at a neutron flux of $2 \times 10^{13} \text{ n/cm}^2 \text{ sec}$ and 10 to 20d decay periods. Detection limits of 120, 2, and 0.5 ng were indicated by measuring respective activities from appropriate photopeaks of ^{59}Fe , ^{51}Cr , and ^{60}Co induced in synthetic standard solution.

The determination of these traces in calcium carbonate is complicated by the decay of the matrix isotope ^{47}Ca . Although the matrix isotope could be allowed to decay before measuring low levels of activity from ^{59}Fe , ^{51}Cr , and ^{60}Co , separating matrix isotopes chemically permits analytical results to be obtained more quickly. Sc and Ca have been removed by extraction with TOPO-cyclohexane and HTTA-TOPO-cyclohexane respectively. Carbonates of sodium and calcium analyzed via these methods have usually shown levels of Cr, Co and Fe below detection limits (Ref. 8).

Instrumental gamma-ray spectroscopy has proven extremely useful for screening high-purity silica because of the favorable nuclear decay of the matrix. Characteristic photopeaks can often be assayed immediately after irradiating the samples. The spectra of the sample in Fig. 6 were recorded 24 hrs. after the end of a 100-hr irradiation. In spectrum A ^{82}Br , ^{24}Na , and ^{51}Cr are visible. After decay of the more abundant shorter lived radionuclides, spectrum B was obtained by counting for 23 minutes. Characteristic photopeaks of ^{59}Fe , ^{60}Co , and ^{51}Cr are more distinct than observed in spectrum A.

Cu and Mn in silica can be determined quantitatively after 15 or 30 min. irradiations and volatilization of ^{31}Si by HF . After 100-hr. irradiations and 2-day decay periods, Cr and Co are assayed nondestructively, while up to 60 day irradiations are necessary to increase detection limits for Fe.

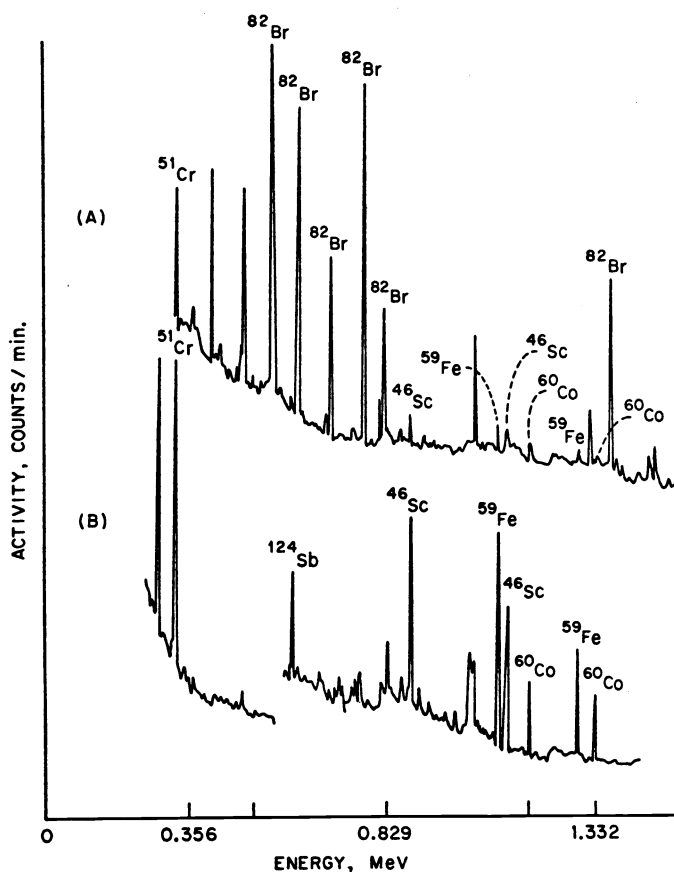


Fig. 6. Gamma-ray spectra of silica

The reliability of instrumental methods should be assessed by analyzing standard reference materials. Results for the analysis of SRM 112 (a silicon carbide) and SRM 85B (an aluminum alloy) are reported in Table 8. Reasonable precision and acceptable accuracy are shown for the determination of relatively large amounts of Fe and Co.

TABLE 8. Fe and Co content of silicon carbide (SRM 112) and aluminum alloy (SRM 85B)^a, $\mu\text{g/g}$

Sample	SRM 112		SRM 85B	
	Fe	Co	Fe	Co
Mean of 6 detn.	4570 ± 230	2.50 ± 0.13	2320 ± 50	1.48 ± 0.03

^aCertified Fe values, SRM 112, 4500 $\mu\text{g/g}$
SRM 85B, 2400 $\mu\text{g/g}$

The precision for iron determinations in SRMs 112 and 85B is $\pm 5\%$ and $\pm 2.1\%$ respectively as measured by relative standard deviations. The average absolute error of the value determined for SRM 112 was 2.5% compared to the recommended NBS value. Based on the certified value for SRM 85B an absolute error of 4.6% occurred. Accuracy of the results for cobalt could not be

assessed since no certified data were available. However, the accuracy of these measurements should be similar to that obtained for iron in view of the comparable precision for cobalt determinations at much lower levels than iron.

Using the instrumental methods described above, measurable limits for trace elements in fused silica were 1.0, 0.1, .01, and 30 ng for Cu, Mn, Co, Cr, and Fe respectively. During most analyses very low levels of Cu and Mn were found. One example of results obtained by neutron activation for the determination of various elements in silica prepared by special procedures is listed subsequently: Cr (0.008 $\mu\text{g/g}$), Co (ND = <0.001 $\mu\text{g/g}$), Cu (0.009 + .004 $\mu\text{g/g}$), Fe (<0.100 $\mu\text{g/g}$), and Mn (0.0089 + .004 $\mu\text{g/g}$). Other results obtained after concentration of trace impurities and measurement by X-ray fluorescence indicated 0.008, 0.001, 0.03-0.09, and <0.01 $\mu\text{g/g}$ of Cr, Co, Cu, and Mn respectively. The supplier's emission spectrographic analysis of this sample after preconcentration of trace elements showed Cr, <0.01; Co, 0.01; Cu, 0.01; Fe, 0.01; Mn, 0.007; Ni, <0.01; and V, <0.01 $\mu\text{g/g}$.

Extremely pure raw materials have been prepared successfully and analyzed by the methods described previously. Additional data for purity characterizations are reported in Tables 9 and 10.

TABLE 9. Transition metal impurities in silica (ng/g)

<u>Sample</u> ^a	<u>Cu</u>	<u>Mn</u>	<u>Co</u>	<u>Cr</u>	<u>Fe</u>
1A	ND	13	1.0	86	ND
B	18	2.0	1.1	17	ND
C	34	5.8	2.2	37	10 ³
2A	50	2.8	1.5	ND	ND
B	41	1.7	1.4	ND	ND
3A	79	2.7	1.0	5.6	ND
B	43	3.4	0.5	ND	ND
C	28	6.3	0.5	ND	ND
C	36	0.5	0.2	2.2	150
4A	35	0.9	ND	1.1	ND
B	12	0.4	ND	1.5	ND
C	15	1.9	ND	1.4	ND
D	45	0.9	ND	ND	ND

^aA, B, C designates separate analyses of various large batches of silica obtained from the same supplier.

The results for these materials are reported in chronological order with respect to the sequence of their preparation in the laboratory. With few exceptions, the results for silica indicate that specifications were being met for Cu, Mn, Co, and Cr. Although no clear trend of increasing purity with time of preparation is seen, silica of extreme purity was obtained routinely. In contrast to the high-purity of silica, samples of the carbonates (Table 9) have Cu (usually above specifications) and periodic Mn contamination. Sodium carbonates [(1) and (2)] and calcium carbonates [(1)-(4)] were prepared during the period in which the purification processes were carefully monitored by analysis at various steps. Preliminary samples were analyzed also prior to the delivery of the large sample. Very low levels of impurities were found in these samples, whereas the remaining samples (Table 10) of sodium carbonate were highly contaminated with Cu. Most of these samples were delivered without any prior analyses.

For quantitative determinations of trace elements in volatile halides, of Si, Ge, P, B and As graphite furnace atomic absorption spectroscopy (AAS) was the

preferred technique.

TABLE 10. Transition metal impurities in waveguide raw materials, (ng/g)

Sample	Cu	Mn	Co	Cr	Fe
Na₂CO₃					
(1)	38 ± 8	46 ± 8	-	-	-
(2)	18.9 ± 7	3.3 ± 1.7	-	-	-
(3)	303	ND	1.0	43.0	ND
(4)	17.7	ND	ND	0.6	ND
(5)	104 ± 4	2.5 ± 0.3	ND	21 ± 2.0	ND
CaCO₃					
(1)	-	-	ND	12 ± 4	ND
(2)	-	-	ND	17 ± 3	ND
(3)	ND	35.7 ± 4.2	-	-	-
(4)	26 ± 6	29.7 ± 1.1	-	-	-
(5)	65	ND	<1	ND	ND
(6)	64 ± 3	3.8 ± 0.2	ND	147	ND

^a Not detected <1.0, <0.1, <0.1, <1.0 and <200 ng for Cu, Mn, Co, Cr, and Fe respectively.

Reliable procedures were developed for processing samples prior to analysis with minimum contamination and without loss of trace elements (Ref. 10). In these reagents iron was the most prevalent impurity and the bulk of all trace transition element impurities was confined to particulate matter contamination in the reagent rather than being solubilized in the liquid reagent. Measurement limits for the AAS technique were \approx 1, 0.3, 0.5, 0.2, 0.5, and 0.5 ng/g for Fe, Cr, Ni, Mn, Cu and Co respectively.

In the sub-ng region quantitative determinations of iron in silicon tetrachloride have been based on laser intracavity absorption spectrometry. An analytically useful laser intracavity spectrometer has been described (Ref. 11) and its application to quantitative determinations of iron has been reported (Ref. 12). A key to the successful exploitation of the inherent sensitivity of the intracavity method for practical analysis was the ultra-purification of analytical buffer and redox reagents used in the spectrophotometric procedures (Refs. 12,13).

CONTAMINATION PROBLEMS

During glass melting

In order to perfect techniques for glass-making material scientists performed exploratory glass-melting experiments using impure reagents. As anticipated, glasses with absorbance losses in the 200-600 dB/Km range were fabricated. The gamma-ray spectrum of a sodium-calcium-silicate glass synthesized from raw materials from a single supplier is given in Fig. 7. The presence of silver was unexpected and both Cr and Co were well above tolerance limits. One of the better optical quality samples (still well above the desired 10 dB/Km), prepared from materials from another source, gave the gamma-ray finger-print shown in Fig. 8. Characteristic photopeaks of ⁵¹Cr, ¹⁹²Ir, ¹²⁴Sb, ⁴⁶Sc, ⁶⁵Zn, and ⁶⁰Co are present in the glass, but no ¹⁹²Ir was detected in any of the spectra of the raw materials used in preparing this sample. Samples of platinum from crucibles used in the melting operation were irradiated and substantial activity ($>10^6$ counts/min per 100 mg of Pt) from ¹⁹²Ir was detected. Gamma-ray spectrometric analysis of glasses melted in an oxygen atmosphere also contained photopeaks of iridium. However, in

nitrogen atmospheres less irridium was detected in the glass. Thus, preparation of glasses by melting in a nitrogen atmosphere reduced contamination from platinum vessels.

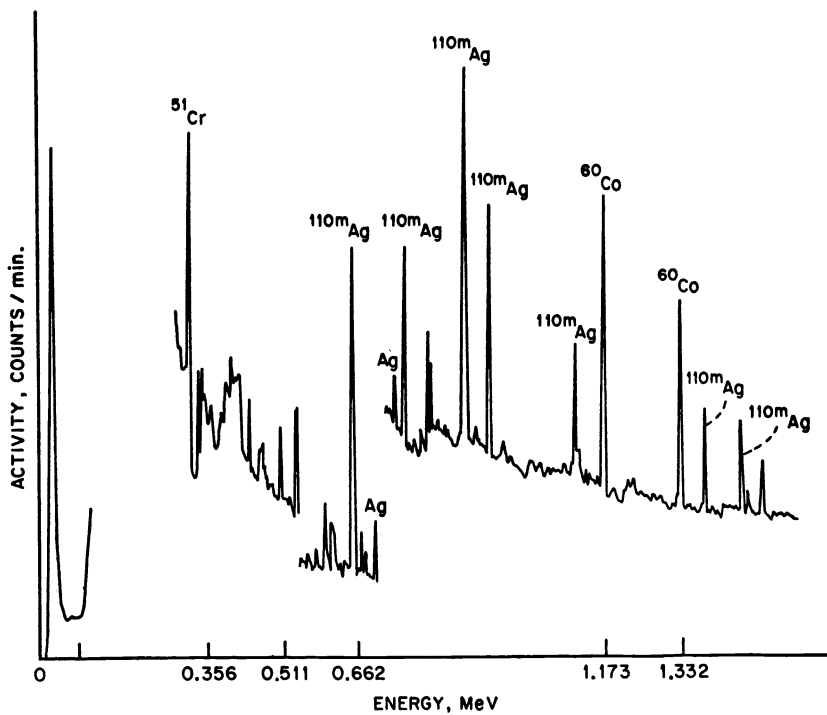


Fig. 7. Gamma-ray spectra of Na-Ca glasses.

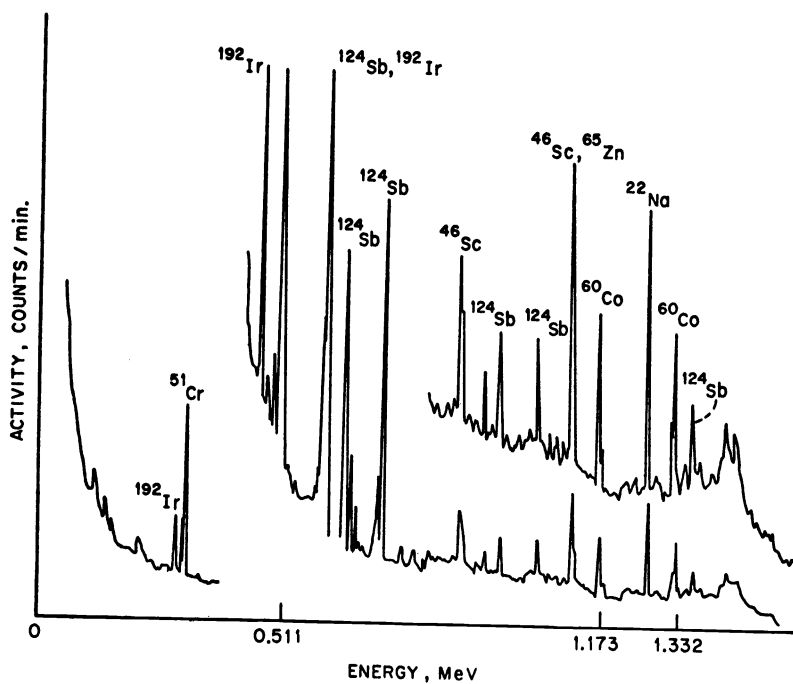


Fig. 8. Gamma-ray spectrum of glass

During fiber production

Modified chemical vapor deposition (MCVD) methods are now being used routinely for the production of preforms from which optical waveguide fibers are drawn (Ref. 5). In this method suitable volatile compounds of silicon plus phosphorus, germanium, or boron are thermally decomposed to form oxide composites inside fused silica tubes. Initially during these investigations some fibers occasionally failed to meet stringent specifications and causative factors were sought by performing neutron activation analyses. The most probable suspects were contaminants present initially in the MCVD starting materials and surface contaminants in the silica tube. The source of optical loss was investigated as follows. Two tubes of approximately equal size (0.63 cm x 8.16 cm), one with a thin film of the CVD deposit, $\text{TiO}_2\text{-SiO}_2$, and the other without were prepared and sealed under the condition existing during the preparation of fiber preforms. These tubes and an aliquot of a standard solution containing known amounts of Na, Mn, Cl and Cu were irradiated simultaneously for twenty minutes. After the irradiation, sample tubes were immersed in 1:1 HNO_3 and rinsed with water to remove any contaminants from the exterior surface. One end of each sealed tube was then carefully opened and each capsule was filled with the same volume of 1:1 HF and HNO_3 . The $\text{TiO}_2\text{-SiO}_2$ thin film was completely dissolved during a 5 minute equilibration at room temperature. Gamma-ray spectra of these solutions are reproduced in Fig. 9(a) and (b).

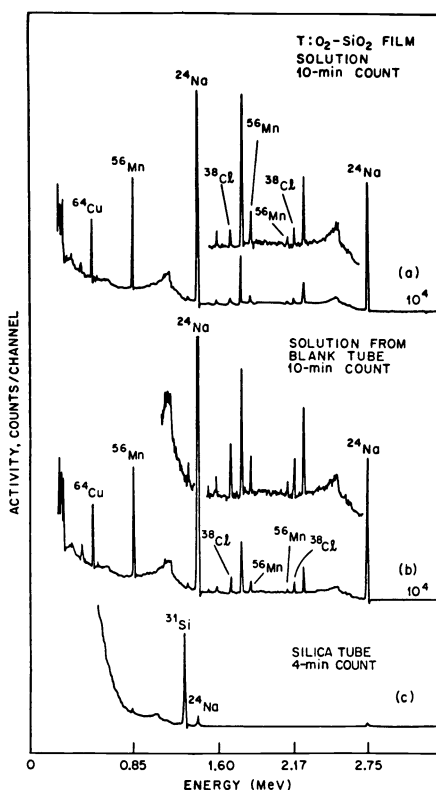


Fig. 9. Gamma-ray spectra of MCVD film, blank and fused silica preform tube.

The solution containing the dissolved film was contaminated with 1.3 μg of Na, 2.5 μg of Mn and 8.6 μg of Cu. Quantities of these impurities in the solution from the blank tubes were Na = 0.93 μg , Mn = 3.2 μg , and Cu = 0.15 μg . Thus, excessive amounts of contamination are present already in the tube prior to deposition of the thin film. A qualitative comparison of the photopeaks in spectrum (c) shows the concentration of impurities in the silica tube to be negligible in comparison to the amounts found in the solutions obtained by rinsing the blank and sample tubes. The results indicated that more thorough cleaning of tubes prior to MCVD was needed. Effective procedures for cleaning fused silica tubes serving as containers for samples during long neutron irradiations have proven to induce negligible amounts of impurities into contained samples (Ref. 8). Similar procedures can be adopted for cleaning fused silica tubes used in MCVD production of waveguides.

In addition to the purity of raw materials and freedom from contamination during the fabrication of bulk glass, it is also necessary to prevent contamination when drawing fibers. On one occasion low loss SiO₂ fibers (~2 dB/Km) were drawn from commercially available pure fused silica and coated with Teflon (FEP). In a subsequent drawing using identical procedures, but with a new furnace, a fiber with a loss over 300 dB/Km was produced. Samples of the acceptable and rejected fiber (15.24 cm lengths x 0.016 cm/dia, sample wt. ~ 40 mg) were activated to identify the impurities responsible for high absorbance losses in the bad fiber. Results (ng/g) for good and bad fibers were respectively Cu, 89 and 311; Mn, 2.2 and 60; and Co <0.1 and 2.2. The Cr and Fe levels in each fiber were below detection limits of 10 and 200 ng respectively. No W was found in the low loss fiber, but 900 ng/g was found in the bad fiber. After stripping the FEP coating from a sample of the high loss fiber and irradiating it, some of the W could be removed by rinsing the fiber in warm 1:1 HNO₃. This suggested that the impurity was probably located at the surface of the fiber and was most likely deposited during drawing. The walls and heating elements of the furnace were contaminated with these impurities.

CONCLUSION

Low loss optical waveguides are now being manufactured routinely under factory conditions in many facilities throughout the world. The rapid progress in development of these systems has been dependent critically on the development of trace analytical techniques for materials characterization and on new purification methods. Analytical chemistry research in these areas continues to be vitally important for industrial growth and technological advancement.

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